

Appendix 1

Algorithm of two-pass phase-shift migration

First pass of conventional downward extrapolation

2-D Fourier transform of stacked section: $P(t, x, \tau=0) \rightarrow P(\omega, k_x)$

For each step $\tau = \Delta\tau, 2\Delta\tau, \dots, \tau_{\max}$:

{

For all k_x :

{

Normal Image: $N(k_x, \tau) = 0$

For $|\omega| > |k_x| v$:

{

$$P(\omega, k_x) = P(\omega, k_x) \times \exp[-i\omega\Delta\tau \sqrt{1 - (vk_x/\omega)^2}]$$

$$N(k_x, \tau) = N(k_x, \tau) + P(\omega, k_x)$$

}

}

1-D inverse Fourier transform: $N(k_x, \tau) \rightarrow N(x, \tau)$

}

Second pass of upward extrapolation

For each step $\tau = \tau_{\max}, \tau_{\max} - \Delta\tau, \dots, \Delta\tau$:

{

For all k_x :

{

Overtuned Image: $O(k_x, \tau) = 0$

For $|k_x| v \leq |\omega| < |k_x| v_{\max}$:

{

$$P(\omega, k_x) = P(\omega, k_x) \times \exp[-i\omega\Delta\tau \sqrt{1 - (vk_x/\omega)^2}]$$

$$O(k_x, \tau) = O(k_x, \tau) + P(\omega, k_x)$$

}

}

1-D inverse Fourier transform: $O(k_x, \tau) \rightarrow O(x, \tau)$

}

Appendix 2

Ray tracing in constant-velocity-gradient media

In a medium with a constant velocity gradient, i.e., velocity defined by

$$v(z) = v_0(1 + \beta z), \quad (\text{A-2-1})$$

rays travel along circular arcs (Slotnick, 1959). Figure A-2.1 shows the geometry of a nonzero-offset recording. Normal reflections are obtained when the reflector angle α is from 0 to 90 degrees, while overturned reflection modeling corresponds to an α between 90 and 180 degrees. The propagating angle θ of a ray is defined as the angle between the ray's direction and the vertical axis. This angle θ is between -180 and $+180$ degrees, and is positive when the ray travels to the right, negative when the ray travels to the left.

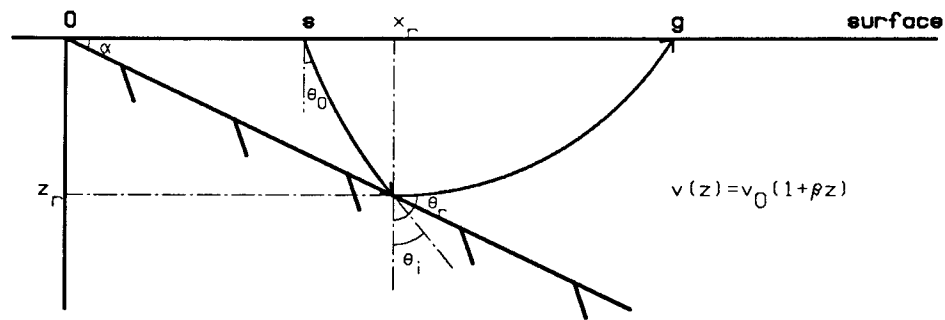


FIG. A-2.1. A nonzero-offset recording geometry. The angle θ_i is the propagating angle of the incident ray at the reflector, while θ_r is the propagating angle of the reflecting ray at the reflector.

The underground position (x, z) through which a particular ray, with a given initial take-off angle θ_0 , passes, and the arrival time of the ray at (x, z) follow (Li et al., 1984):

$$\begin{cases} x = s + \frac{1}{v_0\beta p} \left[\sqrt{1-p^2v_0^2} - \sqrt{1-p^2v^2(z)} \right], \text{ and} \\ t = \frac{1}{v_0\beta} \ln \left(\frac{(1+\beta z) \left[1 + \sqrt{1-p^2v_0^2} \right]}{\left[1 + \sqrt{1-p^2v^2(z)} \right]} \right), \end{cases} \quad (\text{A-2-2})$$

and

$$\begin{cases} x = s + \frac{1}{v_0\beta p} \left[\sqrt{1-p^2v_0^2} + \sqrt{1-p^2v^2(z)} \right], \text{ and} \\ t = \frac{1}{v_0\beta} \ln \left(\frac{\left[1 + \sqrt{1-p^2v_0^2} \right] \left[1 + \sqrt{1-p^2v^2(z)} \right]}{p^2v_0v(z)} \right), \end{cases} \quad (\text{A-2-3})$$

where $p = \sin \theta/v(z) = \sin \theta_0/v_0$ is the ray parameter, and s is the source position on the x axis. Equation (A-2-2) is used if the ray reaches (x, z) before it turns around at its turning point (Li et al., 1984); otherwise equation (A-2-3) should be used.

The reflector's position (x_r, z_r) corresponding to a given ray parameter $p = \sin \theta_0/v_0$ is obtained by solving the following system of equations:

$$\begin{cases} x_r = s + \frac{1}{v_0\beta p} \left[\sqrt{1-p^2v_0^2} \pm \sqrt{1-p^2v_0^2(1+\beta z_r)^2} \right], \text{ and} \\ x_r = \frac{z_r}{\tan \alpha}. \end{cases} \quad (\text{A-2-4})$$

The propagating angle of the reflecting ray at (x_r, z_r) is given by

$$\theta_r = 180^\circ - 2\alpha - \theta_i, \quad (\text{A-2-5})$$

where θ_i can be determined by $\sin \theta_i = v(x_r, z_r)\sin \theta_0/v_0$.

Having determined θ_r , we obtain the ray parameter for the reflecting ray. Thus, the receiver position and the travel time for the reflecting ray can be calculated by equation (A-2-2) or (A-2-3), depending on whether the propagating angle of the ray at the reflector position is larger or smaller than 90 degrees.

Figures A-2.2 and A-2.3 show recording geometries and travel-time curves for a normal reflection and an overturned reflection, respectively. The ray-tracing results

show that time-distance curves for normal reflections and overturned reflections have opposite curvatures in common-shot gathers. The travel-time curve for the normal reflection has a positive second derivative, while that for the overturned reflection is negative.

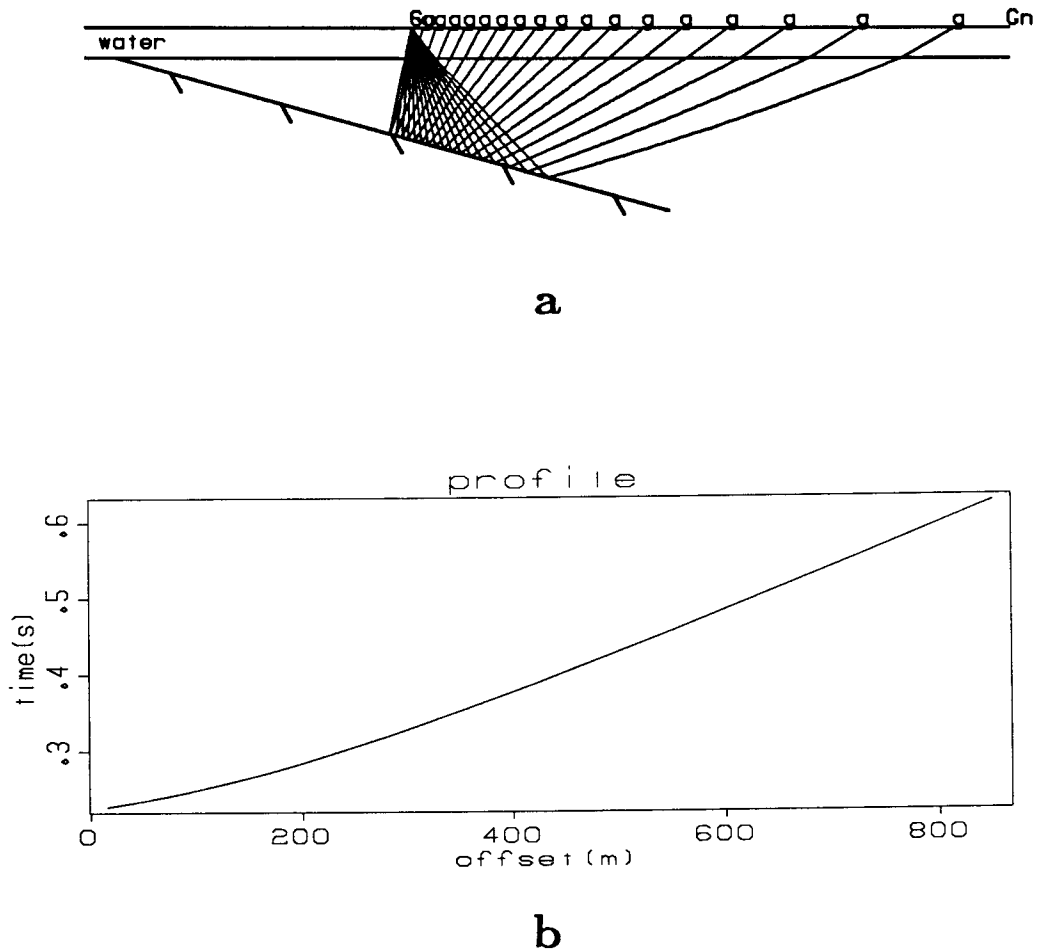
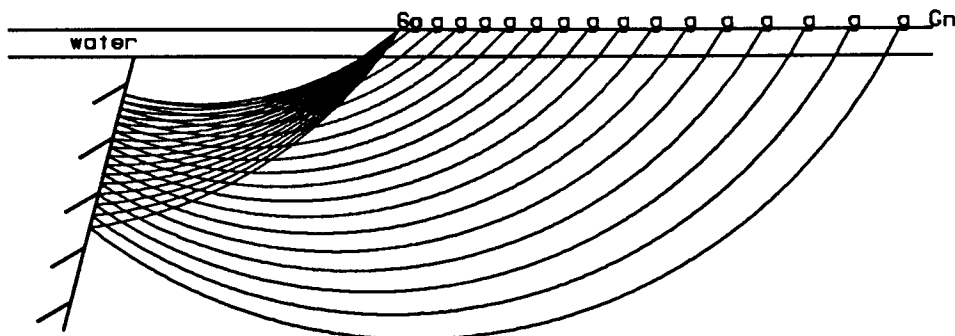
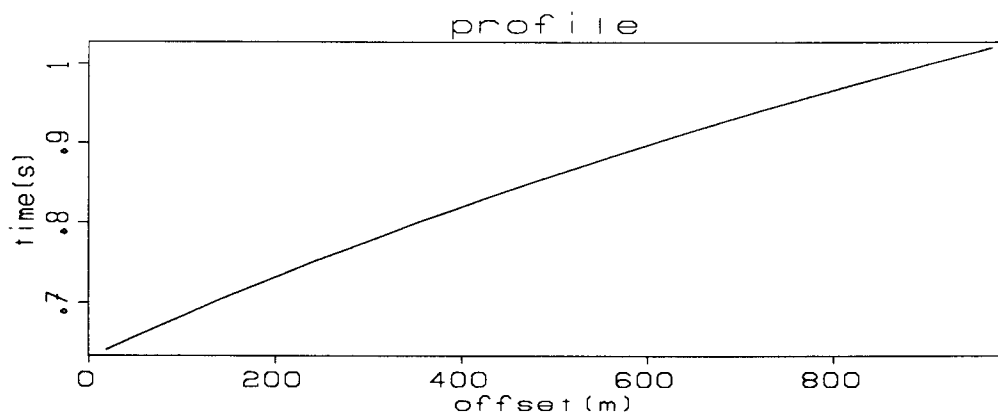


FIG. A-2.2. **a.** Recording geometry for normal reflections. The dip of the reflector α is 15 degrees. The water depth is 50 m and the water velocity is 1500 m/s. The sediment velocity is given by $v(z) = 1600(1+.0002z)$; the shot position is $s = 500$ m; and the cable length is 1000 m. **b.** Travel-time curve of the normal reflections. The curve has positive second derivatives, or curvatures.



a

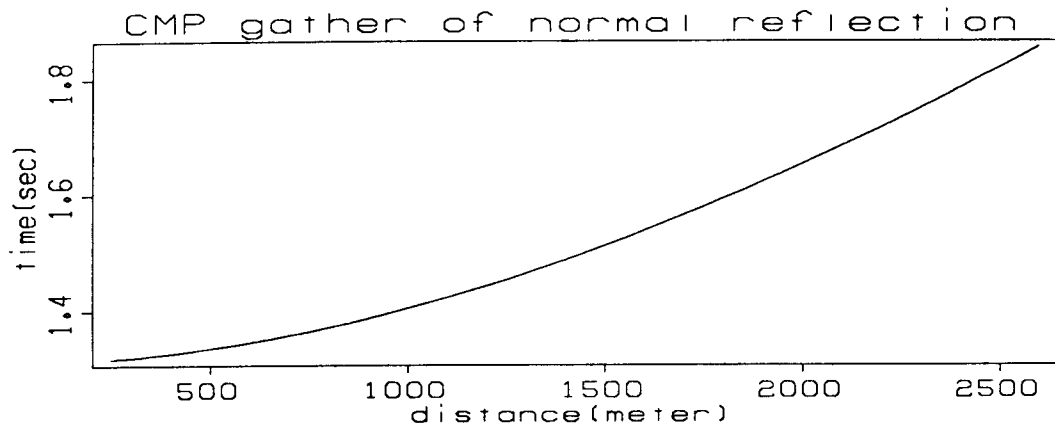


b

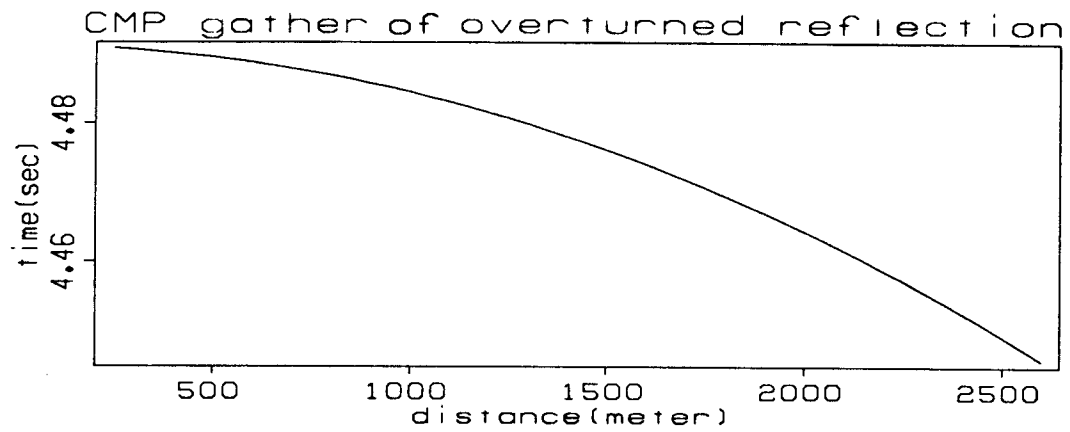
FIG. A-2.3. **a.** Recording geometry for overturned reflections. The dip of the reflector α is 105 degrees. The water depth is 50 m and the water velocity is 1500 m/sec. The sediment velocity is given by $v(z) = 1600(1+.002z)$; the shot position is $s = 500$ m; and the cable length is 1000 m. **b.** Travel-time curve of the normal reflections. The curve has negative second derivatives, or curvatures.

The seismograms generated by the ray-tracing algorithm just described are calculated after scanning over some initial angles, θ_0 's. The time-distance curve is not evenly sampled over the horizontal axis (the geophone axis g). To obtain a common-midpoint gather, interpolation (e.g., spline interpolation) is necessary. Figure A-2.4 shows the common-midpoint gathers for normal reflections and overturned reflections. Opposite moveouts for normal and overturned reflections can be seen in the figure. The travel

times of the overturned reflections in a common-midpoint gather decrease as the offsets increase!



a



b

FIG. A-2.4. **a.** Common-midpoint gather for normal reflections. **b.** Common-midpoint gather for overturned reflections.

Appendix 3

Accuracy and stability of the 1-D characteristic method

The one-dimensional upcoming wave equation can be written as

$$\frac{\partial P}{\partial z} - \frac{1}{v} \frac{\partial P}{\partial t} = 0, \quad (\text{A-3-1})$$

where v is velocity, z depth, and t time.

The leap-frog finite-difference approximation to equation (A-3-1) is

$$P(t_n + \Delta t, z_j) = P(t_n - \Delta t, z_j) + \lambda v [P(t_n, z_j + \Delta z) - P(t_n, z_j - \Delta z)], \quad (\text{A-3-2})$$

where $\lambda = \Delta t / \Delta z$. This method is stable when $\lambda \leq 1$ and is accurate to the second orders of Δt and Δz (Mitchell and Griffiths, 1980).

Applying the characteristic coordinate transformation

$$\begin{cases} \xi = t + z/v \\ \eta = t - z/v \end{cases}, \quad (\text{A-3-3})$$

equation (A-3-1) can be transformed to

$$\frac{\partial P}{\partial \eta} = 0, \quad (\text{A-3-4})$$

The finite-difference method is then

$$P(\eta_n) = P(\eta_n - \Delta \eta) = P(\eta_0). \quad (\text{A-3-5})$$

Clearly, the finite-difference solution of the characteristic equation is exact and unconditionally stable.

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