

Optimized implicit finite-difference migration for VTI media

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SUMMARY

I develop an implicit finite-difference migration method for vertical transversely isotropic (VTI) media with laterally varying anisotropy parameters. I approximate the dispersion relation of VTI media with a rational function series, the coefficients of which are estimated by least-squares optimization. These coefficients are functions of Thomsen anisotropy parameters. They are calculated and stored in a table before the wavefield extrapolation. The implicit finite-difference scheme for VTI media is almost the same as that of the isotropic media, except that the coefficients are derived from the pre-calculated table. In the 3D case, a phase-correction filter is applied after the finite-difference operator to eliminate the numerical-anisotropy error caused by two-way splitting. This finite-difference operator for VTI media is accurate to 60° for the 2nd order approximation and 80° for the 4th order approximation. Its computational cost is almost the same as the isotropic migration. I apply this method to a 2D synthetic dataset to validate the method.

INTRODUCTION

Anisotropy is becoming increasingly important in seismic imaging. If anisotropy is not included in migration, reflectors will not be imaged at the right positions, or even worse, they will be defocused. However, imaging in a general anisotropic medium is still a challenging problem. A vertical transversely isotropic (VTI) medium is one of the simplest and most practical approximations for anisotropic media in seismic imaging. Compared to that of isotropic media, the dispersion relation of VTI media is much more complicated. As a result, phase-shift-based methods (Rousseau, 1997; Ferguson and Margrave, 1998) and explicit convolution methods (Uzcategui, 1995; Zhang et al., 2001a,b; Baumstein and Anderson, 2003; Shan and Biondi, 2005; Ren et al., 2005) are usually used in anisotropic migration, because the complex dispersion relation does not increase the difficulty of these algorithms. However, phase shift with interpolation requires a lot of reference wavefields, because there are two Thomsen anisotropy parameters in addition to the vertical velocity. Explicit convolution methods do not guarantee stability, and they also require long convolution filters to achieve good accuracy.

The implicit finite-difference method has been one of the most attractive migration methods for isotropic media. It can handle lateral variation naturally and guarantee stability. Traditional finite-difference methods, such as the 15° equation (Claerbout, 1971) and the 45° equation (Claerbout, 1985), approximate the dispersion relation by the truncation of Taylor series. Lee and Suh (1985) approximate the square-root equation with rational functions, and optimize the coefficient with least-squares. This can achieve a scheme accurate to 65°. It is much more difficult to design an implicit finite-difference method for VTI media, because of the complicated dispersion relation. Under the weak anisotropy assumption, Ristow and Ruhl (1997) design an implicit scheme for VTI media. Liu et al. (2005) apply a phase-correction operator (Li, 1991) after the finite-difference operator for VTI media and improve the accuracy.

In this paper, I present an optimized one-way wave equation for VTI media and introduce a table-driven, implicit finite-difference method for laterally varying media. I also apply the phase-correction filter to reduce the error. I test the scheme with a synthetic dataset.

OPTIMIZED ONE-WAY WAVE EQUATION OPERATOR FOR VTI

For isotropic media, the dispersion relation for the one-way wave equation

can be represented as

$$\frac{k_z}{\omega/v} = \sqrt{1 - \left(\frac{k_r}{\omega/v}\right)^2}, \quad (1)$$

where ω is the circular frequency, $v = v(x, y, z)$ is the velocity, k_z is the wavenumber, $k_r = \sqrt{k_x^2 + k_y^2}$ is the radial wavenumber, and k_x, k_y are wavenumbers for x and y respectively. Let $S_z = \frac{k_z}{\omega/v}$, and $S_r = \frac{k_r}{\omega/v}$. The square-root function can be approximated by a series of rational functions:

$$S_z \approx 1 - \sum_{i=1}^n \frac{\alpha_i S_r^2}{1 - \beta_i S_r^2}. \quad (2)$$

The coefficients α_i and β_i can be obtained by Taylor-series analysis or rational factorization. If we consider the second-order approximation ($n = 1$) and $\alpha_1 = \frac{1}{2}$, $\beta_1 = \frac{1}{4}$, we obtain the traditional 45° equation. The coefficients α_i and β_i can also be obtained by least-squares optimization, and a more accurate finite-difference scheme like the 65° equation can be obtained (Lee and Suh, 1985).

For VTI media, the true dispersion relation requires solving a quartic equation numerically. With the assumption that the S-wave velocity is much smaller than the P-wave velocity, the dispersion relation for VTI media can be obtained analytically and represented as follows (Tsvankin, 1996):

$$\frac{k_z}{\omega/v_p} = \sqrt{\frac{1 - (1 + 2\varepsilon) \frac{k_r^2}{(\omega/v_p)^2}}{1 - 2(\varepsilon - \delta) \frac{k_r^2}{(\omega/v_p)^2}}}, \quad (3)$$

where $v_p = v_p(x, y, z)$ is the vertical velocity, and $\varepsilon = \varepsilon(x, y, z)$ and $\delta = \delta(x, y, z)$ are the anisotropy parameters defined by Thomsen (1986):

$$\varepsilon = \frac{C_{11} - C_{33}}{2C_{33}}, \delta = \frac{(C_{11} + C_{44})^2 - (C_{33} - C_{44})^2}{2C_{33}(C_{33} - C_{44})},$$

where C_{ij} are elastic stiffness moduli. Let $S_z = \frac{k_z}{\omega/v_p}$ and $S_r = \frac{k_r}{\omega/v_p}$. This dispersion relation can be further simplified under the weak anisotropy assumption, and it can be approximated as

$$S_z \approx 1 - \frac{\alpha_1 S_r^2}{1 - \beta_1 S_r^2}, \quad (4)$$

where $\alpha_1 = 0.5(1 + 2\delta)$ and $\beta_1 = \frac{2(\varepsilon - \delta)}{1 + 2\delta} + 0.25(1 + 2\delta)$ (Ristow and Ruhl, 1997). The coefficients α_1 and β_1 are obtained analytically by Taylor-series analysis.

As in the isotropic case, the coefficients α_i and β_i can also be obtained by least-squares optimization. The advantage of least-squares approximation is that an explicit, analytical expression for the dispersion relation is not required. This is especially useful for anisotropic media. For VTI media, I can use the true dispersion relation, and no assumption of small S-wave velocity or weak anisotropy is necessary.

Generally, the Padé approximation suggests that if the function $S_z(S_r) \in C^{n+m}$, then $S_z(S_r)$ can be approximated by a rational function $R_{n,m}(S_r)$:

$$R_{n,m}(S_r) = \frac{\sum_{i=0}^n a_i S_r^i}{\sum_{i=0}^m b_i S_r^i}, \quad (5)$$

where the coefficients a_i and b_i can be obtained either analytically by Taylor-series analysis or numerically by least-squares fitting.

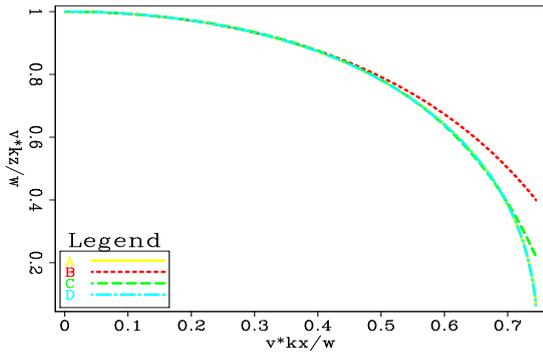


Figure 1: Dispersion relation: curve A is the true dispersion relation; B is the approximate dispersion relation by Taylor-series analysis; C is the approximate dispersion relation by the 2nd order optimization; D is the approximate dispersion relation by the 4th order optimization.

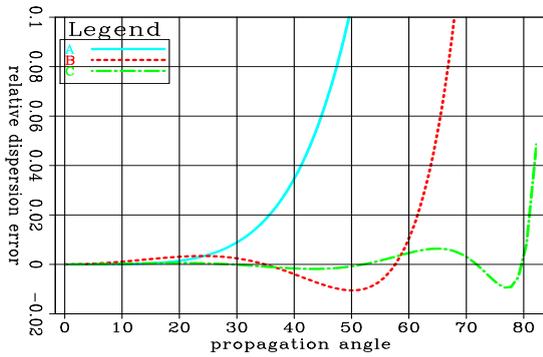


Figure 2: Relative dispersion error: curve A is the relative dispersion error of the approximation by Taylor-series analysis (2nd order); B is the relative dispersion error of the approximation by the 2nd order optimization; C is the relative dispersion error of the approximation by the 4th order optimization.

In VTI media, we can obtain the coefficients a_i and b_i by solving the following optimization problem:

$$\min \int_0^{\sin(\phi)} \left(\sqrt{\frac{1 - (1 + 2\varepsilon)S_r^2}{1 - 2(\varepsilon - \delta)S_r^2}} - \frac{\sum a_i S_r^2}{\sum b_i S_r^2} \right)^2 dS_r, \quad (6)$$

where ϕ is the maximum optimization angle. This problem can be changed to

$$\min \int_0^{\sin(\phi)} \left(\sqrt{\frac{1 - (1 + 2\varepsilon)S_r^2}{1 - 2(\varepsilon - \delta)S_r^2}} \left(\sum_{i=0}^m b_i S_r^2 \right) - \left(\sum_{i=0}^n a_i S_r^2 \right) \right)^2 dS_r. \quad (7)$$

The optimization problem (7) can be solved by a least-squares method. Given ε and δ , we can solve a_i and b_i from equation (7), and we can approximate k_z as follows:

$$k_z \approx \frac{\omega}{v_p} \frac{\sum_{i=0}^n a_i S_r^i}{\sum_{i=0}^m b_i S_r^i}. \quad (8)$$

As Ma (1981) suggested, if $m = n$, equation (8) can be further split into a rational-function series as follows:

$$k_z \approx \frac{\omega}{v_p} \left(1 - \sum_{i=1}^n \frac{\alpha_i S_r^2}{1 - \beta_i S_r^2} \right). \quad (9)$$

The dispersion error of approximation (9) is given by

$$\Delta k_z = \frac{\omega}{v_p} \left[\sqrt{\frac{1 - (1 + 2\varepsilon)S_r^2}{1 - 2(\varepsilon - \delta)S_r^2}} - \left(1 - \sum_{i=1}^n \frac{\alpha_i S_r^2}{1 - \beta_i S_r^2} \right) \right]. \quad (10)$$

The relative dispersion error is defined by $\Delta k_z/k_z$.

Figure 1 shows the true and approximated dispersion relation, given $\varepsilon = 0.4$ and $\delta = 0.2$. In Figure 1, curve A is the true dispersion relation curve. B is the approximated dispersion suggested by Ristow and Ruhl (1997), in which $\alpha_1 = 0.700000$ and $\beta_1 = 0.635714$. C is the approximated dispersion relation by the 2nd order least-squares optimization, in which $\alpha_1 = 0.664820$ and $\beta_1 = 0.948380$. D is the approximated dispersion relation by the 4th order least-squares optimization. The dispersion relation by optimization (C) approximates the true dispersion relation better than the approximation using Taylor-series analysis and the weak anisotropy assumption. The 4th order optimization approximates the true dispersion relation better than the 2nd order optimization.

Figure 2 shows the relative dispersion error. A is the relative dispersion error of the 2nd order approximation using the Taylor-series analysis. B is the relative dispersion error of the 2nd order optimized one-way wave equation operator. C is the relative dispersion error of the 4th order optimized one-way wave equation operator. Figure 2 shows that optimization greatly improves the accuracy of the dispersion relation. If we accept a one-percent dispersion error, the 2nd order optimized one-way wave-equation is accurate to 60° , 4th order optimized one-way wave-equation is accurate to 80° , and the 2nd order approximation using Taylor-series analysis is accurate to only 30° .

TABLE-DRIVEN IMPLICIT FINITE-DIFFERENCE MIGRATION

For the second-order approximation ($m = 1, n = 1$), equation (9) is the following cascaded partial differential equation in the space domain:

$$\frac{\partial}{\partial z} P = i \frac{\omega}{v_p} P, \quad (11)$$

$$\frac{\partial}{\partial z} P = i \frac{\omega}{v_p} \frac{\alpha_1 \frac{v_p^2}{\omega^2} \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right)}{1 + \beta_1 \frac{v_p^2}{\omega^2} \left(\frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2} \right)} P. \quad (12)$$

In isotropic migration, α_1 and β_1 are constant. In VTI media, α_1 and β_1 are functions of the anisotropy parameters ε and δ . For laterally varying media, the value of α_1 and β_1 also vary laterally. It is too expensive to calculate α_1 and β_1 for each grid point during the wave-field extrapolation. I calculate α_1 and β_1 for a range of ε and δ and store them in a table before the migration. I then generate maps of α_1 and β_1 from the table. With the map of the coefficients α_1 and β_1 , the finite-difference scheme for VTI media can be performed in the same way as an isotropic migration.

PHASE CORRECTION FILTER

In the 3D case, as in the isotropic migration, the dispersion relation is split into x and y components as follows:

$$\frac{\partial}{\partial z} P = i \frac{\omega}{v_p} \left[\frac{\alpha_1 \frac{v_p^2}{\omega^2} \frac{\partial^2}{\partial x^2}}{1 + \beta_1 \frac{v_p^2}{\omega^2} \frac{\partial^2}{\partial x^2}} + \frac{\alpha_1 \frac{v_p^2}{\omega^2} \frac{\partial^2}{\partial y^2}}{1 + \beta_1 \frac{v_p^2}{\omega^2} \frac{\partial^2}{\partial y^2}} \right] P. \quad (13)$$

This two-way splitting causes numerical anisotropy, which can be remedied by a phase-correction filter (Li, 1991) in the Fourier domain as follows:

$$P = P e^{i\Delta k_z L}, \quad (14)$$

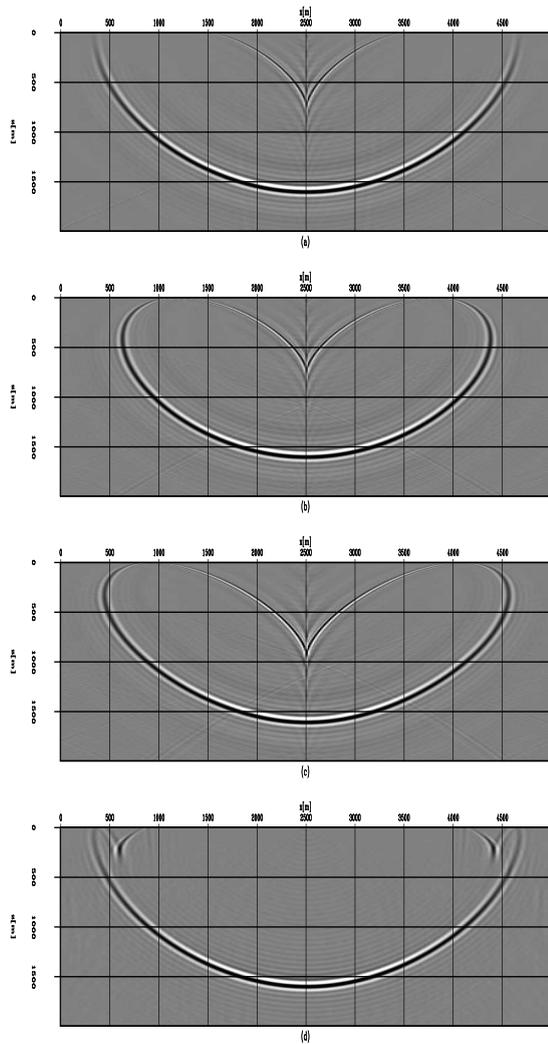


Figure 3: Impulse responses: (a) Phase-shift method; (b) Finite-difference method by Taylor-series analysis (2nd order); (c) 2nd order optimized finite-difference method; (d) 4th order optimized finite-difference method.

where

$$k_L = \sqrt{\frac{1 - (1 + 2\epsilon_r) \frac{k_z^2}{(\omega/v_p^r)^2}}{1 - 2(\epsilon_r - \delta_r) \frac{k_z^2}{(\omega/v_p^r)^2}} - \left[1 - \frac{\alpha_1^r (\frac{\omega}{v_p^r} k_x)^2}{1 - \beta_1^r (\frac{\omega}{v_p^r} k_x)^2} - \frac{\alpha_1^r (\frac{\omega}{v_p^r} k_y)^2}{1 - \beta_1^r (\frac{\omega}{v_p^r} k_y)^2} \right]}, \quad (15)$$

where v_p^r is the reference vertical velocity, ϵ_r and δ_r are the reference anisotropy parameters, and α_1^r and β_1^r are the optimized finite-difference coefficients corresponding to the anisotropy parameters ϵ_r and δ_r .

NUMERICAL EXAMPLES

Impulse response

Figure 3 shows the impulse responses of a homogeneous VTI medium. The vertical velocity of the medium is 2000 m/s, the anisotropy parameter ϵ is 0.4 and the anisotropy parameter δ is 0.2. The travel-time of the impulse is 2 seconds. Figure 3(a) is the impulse response of the

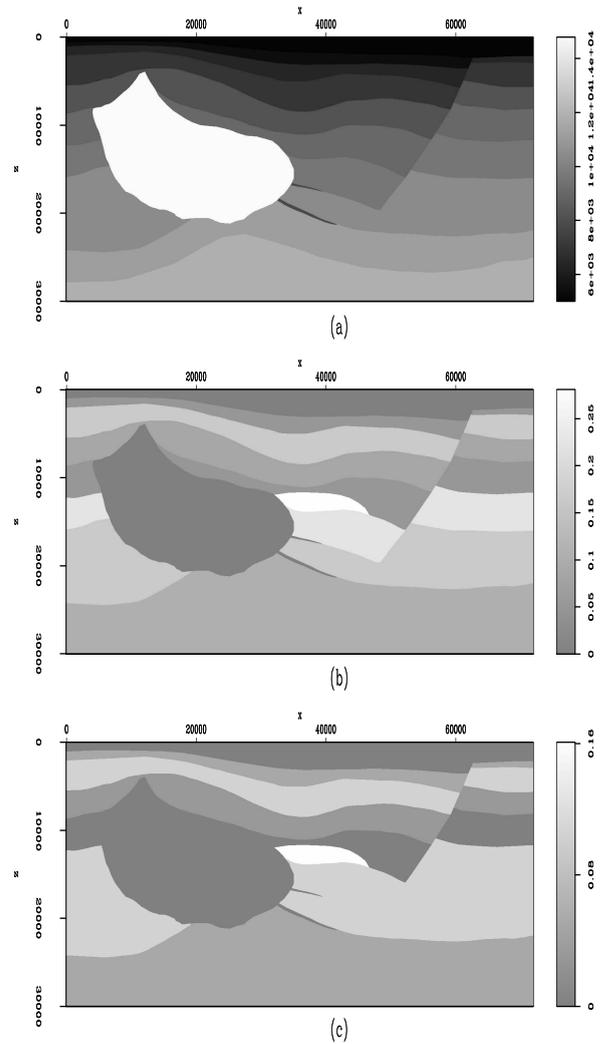


Figure 4: Vertical velocity and anisotropy parameters: (a) vertical velocity; (b) anisotropy parameter ϵ ; (c) anisotropy parameter δ .

phase-shift operator, using equation (3) as the dispersion relation, Figure 3(b) is the impulse response of the finite-difference operator by Taylor-series analysis suggested by Ristow and Ruhl (1997), Figure 3(c) is the impulse response of the 2nd order optimized implicit finite-difference operator, and Figure 3(d) is the impulse response of the 4th order optimized implicit finite-difference operator. From Figure 3, we can see that with the same order approximation the impulse response of the optimized implicit finite-difference operator (Figure 3(c)) is more accurate than the impulse response from Taylor-series analysis (Figure 3(b)). The impulse response in Figure 3(c) is accurate to 60° , while the impulse response in Figure 3(b) is accurate to only 30° . The 4th order optimized finite-difference operator (Figure 3(d)) is more accurate than the 2nd order optimized finite-difference operator (Figure 3(c)). The impulse responses also verify the relative-dispersion-relation error analysis in Figure 2.

A synthetic dataset

Figures 4 show a synthetic model for VTI media. Figure 4(a) is the velocity model, Figure 4(b) is the map of the anisotropy parameter ϵ , and Figure 4(c) is the map of the anisotropy parameter δ . There are 720 shots in total and the maximum offset for each shot is 8000 meters.

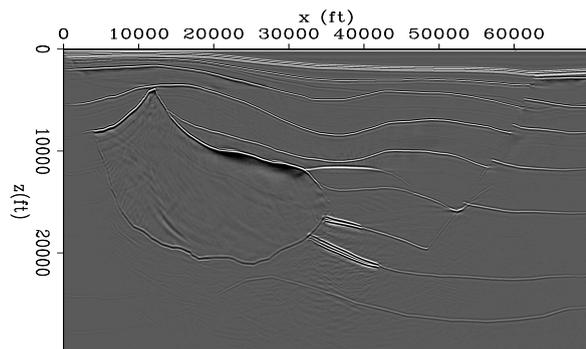


Figure 5: The 2nd order optimized finite-difference migration.

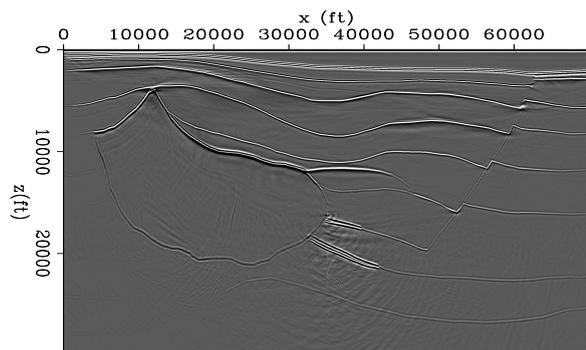


Figure 6: The 4th order optimized finite-difference migration.

The challenging part of this model is to accurately image the steep fault, salt flank and the two abnormal sediments near the right corner of the salt body. I run a plane-wave migration, using the optimized implicit finite-difference operator as the extrapolator. I generate 70 plane-wave sources, for which the take-off angles at the surface range from -40° to 40° . Figure 5 shows the image obtained by the 2nd order optimized finite-difference method. Notice that the steeply dipping salt flank and the fault are well imaged. The abnormal sediments also are well imaged. Figure 6 shows the image obtained by the 4th order optimized finite-difference method. Compared to the 2nd order optimized finite-difference, the 4th order optimized finite-difference improves the steeply dipping salt flank and the fault.

CONCLUSION

I present an implicit finite-difference migration method for VTI media. The scheme is designed by approximating the dispersion relation with rational functions and solving the coefficients by least-squares methods. The coefficients of finite-difference are obtained from a table, which is calculated before the wavefield extrapolation. This implicit finite-difference method guarantees stability, and its computational cost is almost the same as isotropic implicit finite-difference migration. Both dispersion-error analysis and impulse response indicate that the implicit finite-difference operator is accurate to 60° for the 2nd order optimization and 80° for the 4th order optimization. The migrations for the synthetic dataset show that this implicit finite-difference method can extrapolate the wavefield accurately in laterally varying media.

ACKNOWLEDGMENTS

I would like to thank Faqi Liu from Amerada Hess for useful discussions. I would like to thank Amerada Hess for making the synthetic

dataset available. I would like to thank all the sponsors of the Stanford Exploration Project for financial support.

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